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PARKSIDE GREATER ASCOT DALRYMPLE ROAD, SHAW CLIENT - PARKSIDE DEVELOPMENTS

3D DRAWING & RENDERS - CARWASH SHEET 01 03 STAGE 1 ISSUE
02 FOR INFOMATION
01 PROGRESS ISSUE
ISSUE PURPOSE 7/11/24 CPA EB MC 19/09/24 CPA EB MC 30/08/24 CPA EB MC DATE D C A JOB No 6570 SD SD0211

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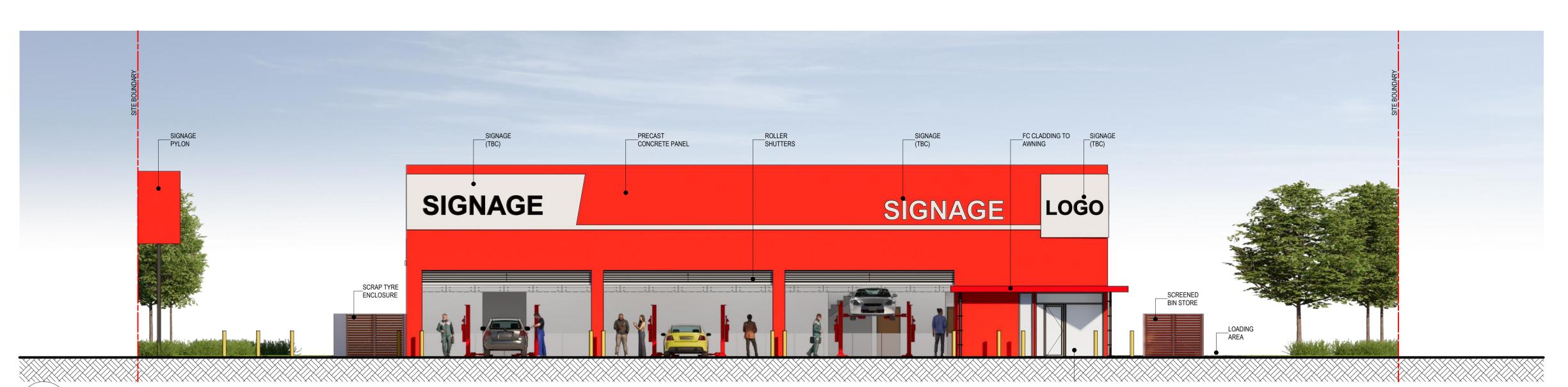
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TYRE AND AUTO CENTRE EAST ELEVATION

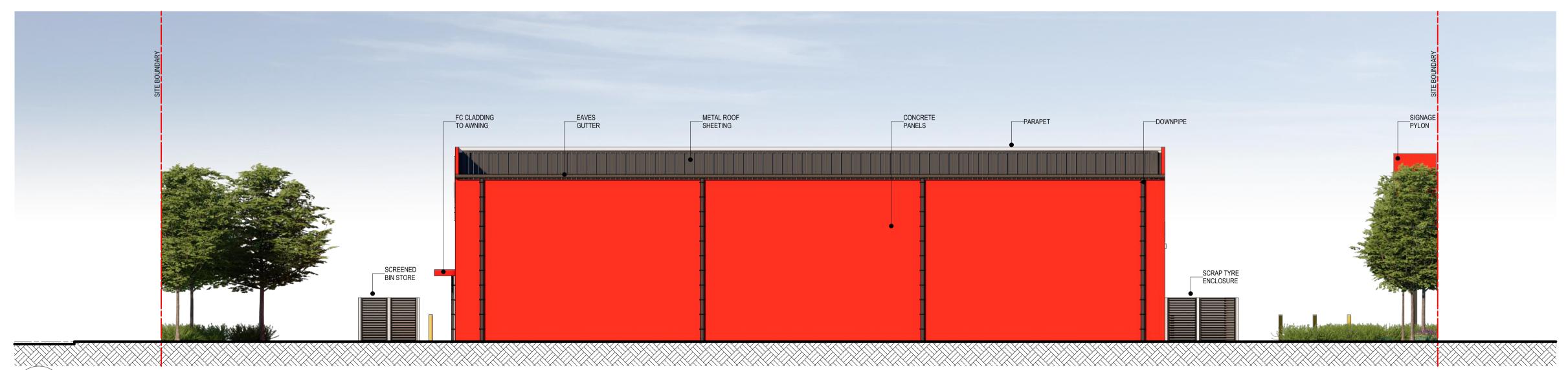
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2 TYRE AND AUTO CENTRE NORTH ELEVATION

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TYRE AND AUTO CENTRE WEST ELEVATION SCALE 1:100 @ A1 SCALE 1:200 @ A3

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DALRYMPLE ROAD, SHAW CLIENT - PARKSIDE DEVELOPMENTS DRAWING TITLE TYRE AND AUTO CENTRE ELEVATIONS

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PARKSIDE GREATER ASCOT

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DALRYMPLE ROAD, SHAW

CLIENT - PARKSIDE DEVELOPMENTS

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DALRYMPLE ROAD, SHAW

CLIENT - PARKSIDE DEVELOPMENTS

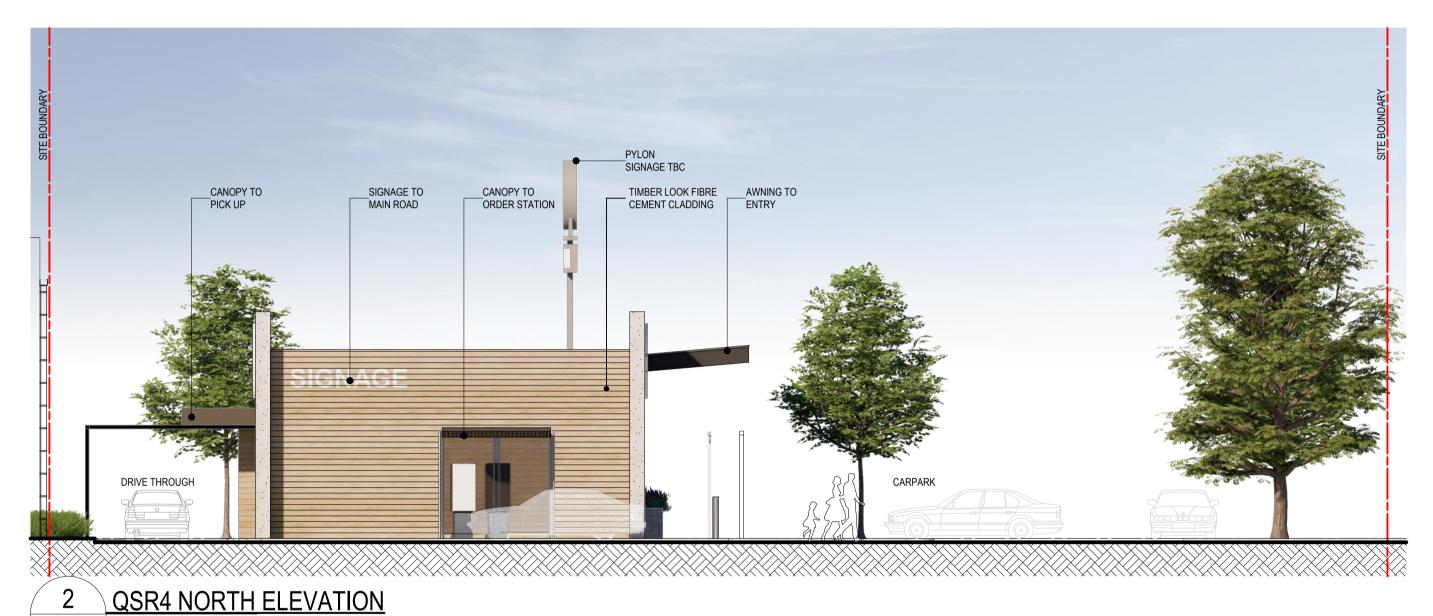
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4 QSR4 EAST ELEVATION

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PARKSIDE GREATER ASCOT

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DALRYMPLE ROAD, SHAW CLIENT - PARKSIDE DEVELOPMENTS

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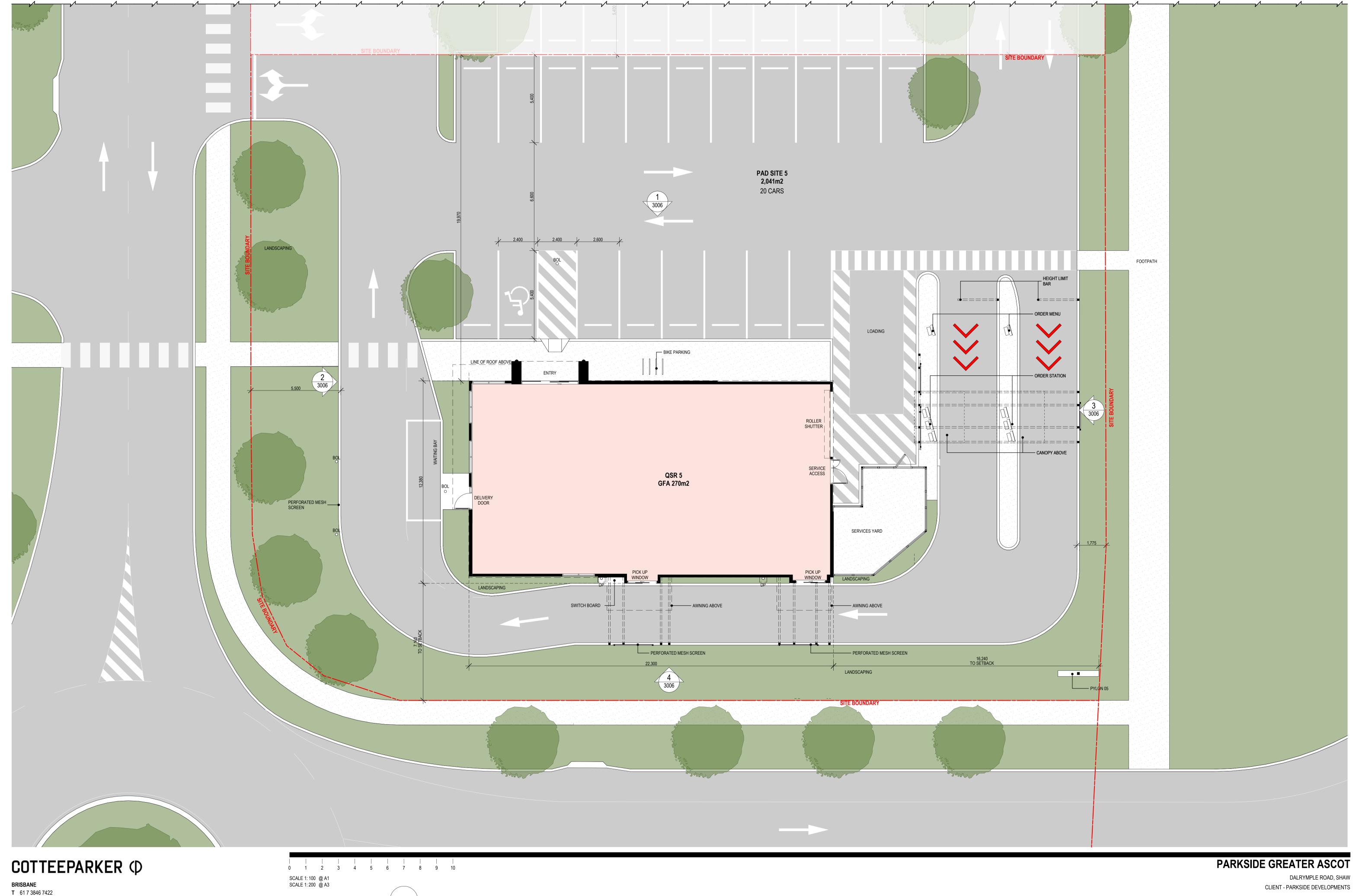
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CLIENT - PARKSIDE DEVELOPMENTS

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DALRYMPLE ROAD, SHAW CLIENT - PARKSIDE DEVELOPMENTS

QSR 5 FLOOR PLAN



QSR 5 EAST ELEVATION

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FIBRE CEMENT
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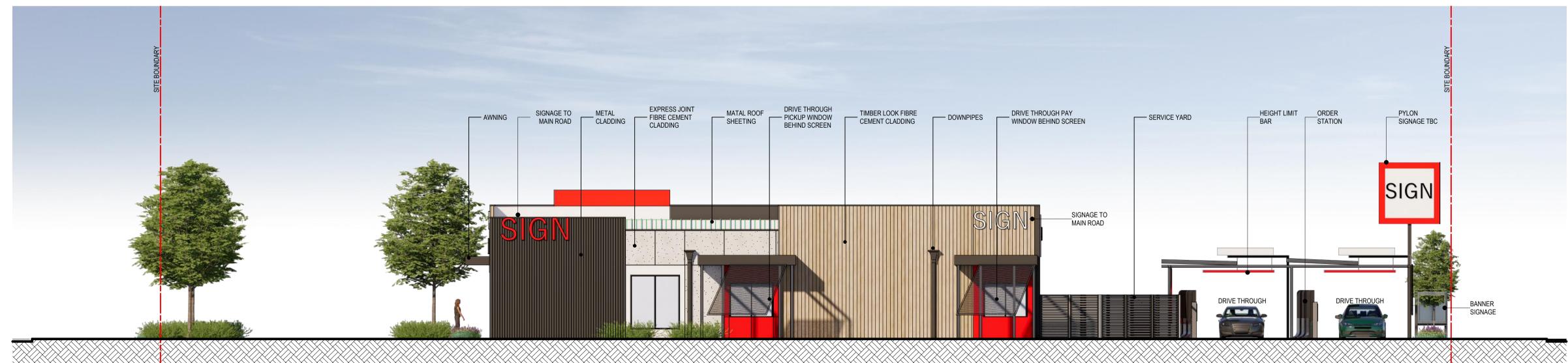
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QSR 5 NORTH ELEVATION

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3 QSR 5 SOUTH ELEVATION

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QSR 5 WEST ELEVATION SCALE 1:100 @ A1 SCALE 1:200 @ A3

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DALRYMPLE ROAD, SHAW

CLIENT - PARKSIDE DEVELOPMENTS

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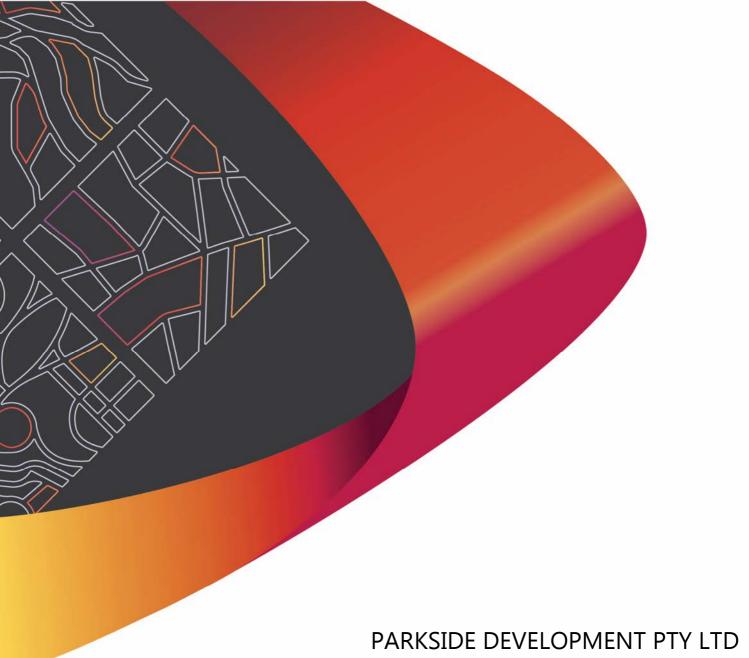
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APPENDIX E

Engineering Report prepared by Premise





GREATER ASCOT TOWN CENTRE STAGE 1

ENGINEERING REPORT

Report No: P001406.R02

Rev: A

8 November 2024



Document Set ID: 26515272 Version: 1, Version Date: 18/11/2024



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DOCUMENT AUTHORISATION					
Revision	Revision Date	Proposal Details			
А	08/11/24	For Approval			
Prepared By		Reviewed By		Authorised By	
Zac Strogusz	3 glass	Zac Strogusz	3 glnes	Katie De Lacey	M

Document Set ID: 26515272 Version: 1, Version Date: 18/11/2024



CONTENTS

1.	INTRODUCTION	2
2.	PROPOSED DEVELOPMENT	3
3.	TRAFFIC AND ROADWAYS	4
3.1	Development Access	4
3.2	External Road Network	4
3.3	Internal Road Network	4
4.	ALLOTMENTS AND EARTHWORKS	4
4.1	Existing Vegetation	4
4.2	Existing Ground Conditions	4
4.3	Required Earthworks	5
5.	STORMWATER AND DRAINAGE	5
5.1	Internal Drainage	5
5.2	Water Quality	5
6.	WATER RETICULATION	6
6.1	Water Infrastructure Assessment	6
6.2	Reticulation Mains	7
1.1	Water Demands	7
1.2	Water Network Analysis	9
7.	SEWERAGE INFRASTRUCTURE	9
1.3	Sewer Demands	10
7.1	Sewerage Design Criteria	11
8.	PATHS AND PEDESTRIANS	11
9.	ELECTRICITY AND COMMUNICATIONS	12
10.	CONCLUSION	13
APPI	ENDICES	ERROR! BOOKMARK NOT DEFINED.
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	BLES	
	e 1 - Equivalent Population (EP) Assessment - Water	
	e 2 – Design Parameters – Water Demands	
	e 3 – Water Demands(ED) Assessment - Water	
	e 4 - Equivalent Population (EP) Assessment - Water e 5 – Design Parameters – Sewage Demands	
	e 6 – Sewer Demands	11





FIGURES

Figure 1 – Site Location	2
Figure 2 Proposed Development Architectural Layout	3
Figure 3 – Existing Trunk Water Infrastructure in Site Vicinity	6
Figure 4 – Existing Water Reticulation Infrastructure in Site Vicinity	7
Figure 5 – Existing Sewer Infrastructure in Vicinity of the Proposed Development	10
Figure 6 – Existing Electrical Assets in Site Vicinity	12

Document Set ID: 26515272 Version: 1, Version Date: 18/11/2024



1. INTRODUCTION

Premise have been commissioned by Parkside Development Pty Ltd to prepare this Engineering Report in support of a development application for the Greater Ascot Town Centre Stage 1. The existing site is located at 890 Dalrymple Road (Lot 2 on SP 107219), as shown in Figure 1. This report is to accompany a Material Change of Use application (MCU) of the lot to allow stage 1 of a multistage town centre precinct to be developed.



Figure 1 - Site Location

The proposed development (Stage 1) includes earthworks, sewer and water reticulation, stormwater drainage, roadworks, and electrical and telecommunication works. Stormwater quality objectives are addressed via a standalone report in Appendix E.

The proposed development site is adjacent to the residential component of Greater Ascot Development and bound by Dalrymple Road to the south. West of the site is Shaw Road.



2. PROPOSED DEVELOPMENT

The architectural layouts by Cotter Parker, illustrating the proposed commercial precinct are attached in Appendix A. An extract of this layout is shown below in Figure 2:



Figure 2 Proposed Development Architectural Layout

The proposed development consisting of Stage 1 of the precinct is expected to include:

- > A service station, including a convenience store and carwash, with a Gross Floor Area (GFA) of 385 m².
- > A car service centre of with a GFA of 371 m².
- > Two (2) fast-food restaurants with a combined total GFA of 533 m².
- > A childcare centre site with a total area of 3,248 m².
- > Four (4) pad sites with a combined area of 9,497 m².

The proposed development will also consist of an internal road network consisting of two (2) roundabouts.



3. TRAFFIC AND ROADWAYS

3.1 Development Access

Access to Stage 1 is proposed to be from two (2) accesses from the southern site boundary via Dalrymple Road. This includes a western and an eastern access as shown in the development site plan in Appendix B and reproduced in Figure 2.

3.2 External Road Network

Dalrymple Road is an existing Local Government Road under the governing authority of Townsville City Council (TCC), comprising two lanes in each direction.

Bishop Putney Road is located to the south of the site forming a priority-controlled T-intersection with Dalrymple Road, providing access to and from St Benedict's Catholic School. Upon completion of Stage 1, this intersection will become a four-way signalized intersection, providing access to the development via the northern leg.

3.3 Internal Road Network

The internal road network will be designed to service the development in accordance with the Road pavement shall be designed in accordance with Council Standards. The eastern access will be a Major Collector-Main Street. The Road Hierarchy and typical cross section is shown on Premise Sketch P001406/SKC01 and is attached in Appendix A.

Road pavements will be designed and constructed in accordance with Council Standards and policy for commercial type roads based on site geotechnical testing. All line marking and signage requirements shall be in accordance with the Manual of Uniform Traffic Control Devices.

4. ALLOTMENTS AND EARTHWORKS

4.1 Existing Vegetation

The subject site comprises an approximate area of 2.2 Ha and is currently unoccupied. The site is classified as an area of High Environmental Importance under the Townsville City Council Planning Scheme Environmental Importance Overlay (OM-08.0). However, the site is devoid of vegetation classified as a Matter of Environmental Significance (MSES) under the State Planning Policy (2017). Furthermore, recent aerial mapping confirms that the site has been cleared and is devoid of any substantial vegetation.

4.2 Existing Ground Conditions

The site for Stage 1 of the development is relatively flat, with minimal variation between existing surface elevations which range from 13 to 12m AHD. As the site is located between 5-20 m AHD, the risk of encountering Acid Sulfate Soils is considered low.



4.3 Required Earthworks

The site shall be shaped to ensure positive drainage towards roadways or drainage reserves. Grading will be in accordance with Council requirements for non-residential allotments. The subject site shall be filled to a 100-year flood immunity standard in accordance with the current Townsville City Council Planning Scheme Policy Development Manual and State Government requirements. All allotment earthworks shall be carried out to Level 1 testing and inspection by a NATA registered geotechnical inspection and testing authority.

5. STORMWATER AND DRAINAGE

Stormwater drainage shall be designed and constructed in accordance with the Townsville City Plan – Planning Scheme Policy – Schedule 6.4.4.4 Stormwater Drainage Design and associated reference documents.

The development will be shaped to ensure positive drainage towards roadways or drainage reserves (ultimately east) as per Council requirements. A preliminary layout of the stormwater strategy is included in Appendix E.

5.1 Internal Drainage

Minor system (Principal Centre (CBD) Q10 - 10% AEP) stormwater flows shall be collected from buildings and carparks and transported via roadway kerb and channel, inverts, and kerb inlet pits and underground stormwater drainage pipes to the roads stormwater system before being discharged to the major drainage system as per Council standards. The major drainage system is the temporary existing open drain that diverts around Greater Ascot Town Centre Stage 1, into the permanent existing drain to the east, and ultimately to the Bohle River.

Major system (Q100 - 1% AEP) stormwater flows, surplus to the minor system capacity, shall be transported via the roadway systems to the main drainage paths, and discharged as per normal Council requirements.

The existing small stormwater catchment from the western side of Shaw Road which discharges under Shaw Road and, the balance of the commercial site, has been allowed to be diverted around stage 1 into the existing temporary drain which diverts around stage 1.

5.2 Stormwater Quality Management Plan

Water Sensitive Urban Design (WSUD) techniques and solutions shall be confirmed during detailed design of the proposed development to ensure adverse impacts are minimalised. A Stormwater Quality Management report has been prepared for the proposed development and is attached as a standalone Report in Appendix E.



6. WATER RETICULATION

6.1 Water Infrastructure Assessment

Existing water infrastructure services in the vicinity of the proposed development site are shown in Figure 3. As shown, there is currently a DN500 trunk main which runs parallel to the southern side of the Dalrymple Road Reserve.



Figure 3 – Existing Trunk Water Infrastructure in Site Vicinity

The existing reticulation within the vicinity of the development is shown in Figure 4 and 4 and the preliminary water sketch on Appendix C. There is an existing DN250 water main which runs along the frontage of the proposed development site, and connects to the existing DN500 trunk main on Dalrymple Road.

The segment running to the north of the site (eastern site boundary) is a temporary installation and is located within the neighbouring eastern lot. This main will be truncated and replaced by a new ultimate main which is within development Road Reserve. Refer to the preliminary water sketch in Appendix C.

PAGE 6 | GREATER ASCOT TOWN CENTRE STAGE 1





Figure 4 - Existing Water Reticulation Infrastructure in Site Vicinity

6.2 Reticulation Mains

The development will be provided with a reticulated water supply, connecting to the existing DN250 main shown in Figure 4. A conceptual water network layout is shown in Appendix C.

Each Easement or Lot within the proposed development shall be serviced via water mains of DN150 PVC . DN150 PVC water mains will generally be on a 1.8m alignment from the property boundary. Valves and hydrants shall be provided in accordance with normal Council requirements.

A hydraulic model for the proposed water network has been developed using WaterCAD, with a model output report included in Appendix G.

1.1 Water Demands

An evaluation of likely demands attributable to the proposed development has been undertaken. The Equivalent Population (EP) for each commercial site within the development site is shown in Table 1. A Loading rate is of 56.8 EP/Ha has been adopted as per Table SC3.1.6a of the Townsville City Plan.

PAGE 7 | GREATER ASCOT TOWN CENTRE STAGE 1

Table 1 - Equivalent Population (EP) Assessment - Water

Land Use	Area (Ha)	Loading Rate (Water)	Equivalent Population (EP)
KFC	0.23	56.8 EP/Ha	13
Food/Drink	0.21	56.8 EP/Ha	12
Tyre and Auto Centre	0.18	56.8 EP/Ha	10
Service Station	0.47	56.8 EP/Ha	27
Childcare	0.32	56.8 EP/Ha	19
Total	1.40		81

The CTM Water Alliance Design and Construction Code (2020) have been used to estimate the likely average day demand and peak hour and mean day maximum month that will apply to the overall development site for water assessment works.

Table 2 presents a summary of the relevant Townsville City Council demand parameters that apply to new and existing developments in the local region.

Table 2 – Design Parameters – Water Demands

Parameter	Adopted Value	
Demands		
Average Day Demand	600 L/EP/day	
Mean Day Maximum Month to Average Day (MDMM / AD) Ratio	1.5	
Peak Hour to Average Day Demand (PH/AD) Ratio	2.81	
Fire Fighting – Commercial	Fire demand 30 L/s over 4h duration, with concurrent Peak Hour background demand	
Service Pressures		
Minimum	22 m at property boundary	
Maximum	80 m	
Emergency Fire Operating Conditions (Minimum Residual Mains Pressures)	12 m at flowing hydrant 6 m elsewhere in mains that have customer connection.	

The water demands for each commercial site within the development are presented in Table 3.

Table 3 – Water Demands

Land Use	Equivalent Population (EP)	Average Day Demand (AD)	Mean Day Maximum Month (MDMM)	Peak Hour (PH)
KFC	13	0.10	0.15	0.28
Food/Drink	12	0.09	0.14	0.26
Tyre and Auto Centre	10	0.08	0.11	0.21
Service Station	27	0.21	0.31	0.58
Childcare	19	0.15	0.22	0.41

PAGE 8 | GREATER ASCOT TOWN CENTRE STAGE 1



7	
Total 81 0.62 0.93	1.74

Based on the population assessment of 81 EP and the above demand parameters, the peak hour demand would be up to 1.74L/s plus firefighting.

1.2 Water Network Analysis

A hydraulic analysis was undertaken to assess the necessary infrastructure required to service the development. A WaterCAD model has been developed for Greater Ascott Town Centre (file name "P001406 Greater Ascott Town Centre Stage 1 WaterCAD") for use in the water supply hydraulic assessment for the development.

The water network modelling assessment demonstrated:

- > The standard scenario had a maximum pressure of 41m throughout the proposed reticulation network, which is well below the desired maximum service pressure of 80 m.
- > The firefighting scenario had a maximum pressure of 41 m and a minimum pressure of 35 m, demonstrating ample pressure will be available.

The attached WaterCAD model output in Appendix G shows the proposed layout of the water network and reticulation mains required for the proposed development.

7. SEWERAGE INFRASTRUCTURE

Existing sewerage services within the vicinity of the proposed development are shown in Figure 5 (and in Appendix D). There are currently no trunk mains located within the Dalrymple road reserve. There is an existing DN300 gravity main located approximately 140 m to the northeast of the site. This main directs flow east along Blackmoor Promenade, across Greater Ascot Avenue and along Huntsmans Cresent to a Sewage Pumping Station on the northern side of Dalrymple Road. This Town Centre development will connect into this existing DN300 gravity main.



PROPOSED DEVELOPMENT SEWER CONNECTION POINT)

EXISTING DIASO
TRUNK MAIN)

DALRYMPLE ROAD

EXISTING DIASO
RISING MAIN

Source: Townsville MAPS - LGIP

Figure 5 - Existing Sewer Infrastructure in Vicinity of the Proposed Development

1.3 Sewer Demands

An evaluation of likely sewer demands attributable to the proposed development has been undertaken. The Equivalent Population (EP) for each commercial site within the development site is shown in Table 1. A Loading rate is of 57.3 EP/Ha (Sewage) has been adopted as per Table SC3.1.6a of the Townsville City Plan.

Land Use	Area (Ha)	Loading Rate (Water)	Equivalent Population (EP)
KFC	0.23	57.3 EP/Ha	13
Food/Drink	0.21	57.3 EP/Ha	12
Tyre and Auto Centre	0.18	57.3 EP/Ha	11
Service Station	0.47	57.3 EP/Ha	27
Childcare	0.32	57.3 EP/Ha	19
Total	1.40		82

Table 4 - Equivalent Population (EP) Assessment - Water

The CTM Water Alliance Design and Construction Code (2020) have been used to establish the likely average dry weather flow (ADWF), peak dry weather flow (PDWF) and peak wet weather flow (PWWF) that will apply to the overall development site for the sewer assessment works. Table 5 presents a summary of the relevant Townsville City Council demand parameters that apply to new and existing developments in the local region.



Table 5 – Design Parameters – Sewage Demands

Parameter	Adopted Value
Average Day Weather Flow (ADWF)	230 L/EP/day
Peak Dry Weather Flow (PDWF)	4.7*EP^(-0.105)*ADWF
Peak Wet Weather Flow (PWWF)	5*ADWF

The sewer demands for each commercial site within the development are presented in Table 6.

Table 6 - Sewer Demands

Land Use	Equivalent Population (EP)	Average Dry Weather Flow (ADWF)	Peak Dry Weather Flow (PDWF)	Peak Wet Weather Flow (PWWF)
KFC	13	0.03	0.12	0.17
Food/Drink	12	0.03	0.12	0.16
Tyre and Auto Centre	10	0.03	0.11	0.15
Service Station	27	0.07	0.24	0.36
Childcare	19	0.05	0.17	0.25
Total	82	0.22	0.76	1.09

Based on the population assessment of 82 EP and the above demand parameters, the peak wet weather flow would be up to 1.09L/s.

7.1 Sewerage Design Criteria

A conceptual sewer layout is shown on Premise Sketch p001406-SKC04 in Appendix D. The proposed gravity sewer line will direct flows north to the existing DN300 trunk main shown in Figure 5.

The sewerage network shall be designed and constructed in accordance with the Townsville City Plan – Planning Scheme Policy and Water Systems Australia Specification WSA-03.

The location and sizing of the internal sewerage infrastructure will be verified as part of the detailed design of the development planning approvals.

8. PATHS AND PEDESTRIANS

There are currently no active transport facilities fronting the existing lot boundary. There is a pathway located on the southern side of the Dalrymple Road Reserve (under construction). This provides a route for pedestrians to access St Benedict's Catholic School from the east by crossing Bishop Putney Road.

To assist in pedestrian circulation through development, it is proposed to construct a new concrete pathway network. The pedestrian pathway network for the development is shown in the architectural

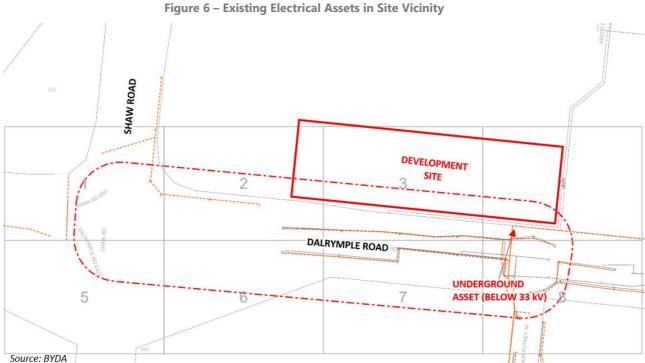
PAGE 11 | GREATER ASCOT TOWN CENTRE STAGE 1



layouts in Appendix B and will be fully considered as part of detailed design. This pathway network will run adjacent the southern site boundary, providing connectivity from the eastern residences and pedestrians crossing from Bishop Putney Road to the south.

9. **ELECTRICITY AND COMMUNICATIONS**

A search of Before You Dig Australia (BYDA) has been undertaken to identify existing underground electrical and telecommunications in the site vicinity. As shown in Figure 6, Ergon administers electrical assets (below 33 kV) in the Dalrymple Road reserve. The closest existing electrical cable to the site is located near the northeast corner of the existing lot boundary, which crosses Dalrymple Road to before continuing along the western side of Bishop Putney Road.



Furthermore, is also an NBN line located on the southern side of Dalrymple Road opposite the site with two pits located either side of the intersection between Bishop Putney Road.

Negotiations shall be undertaken with utility service providers for the supply of electricity and telecommunications to the development. Any electrical reticulation design for the proposed internal works will be completed by a qualified Electrical Engineer during the detailed design phase, and all appropriate approvals sought from the relevant authority.



10. CONCLUSION

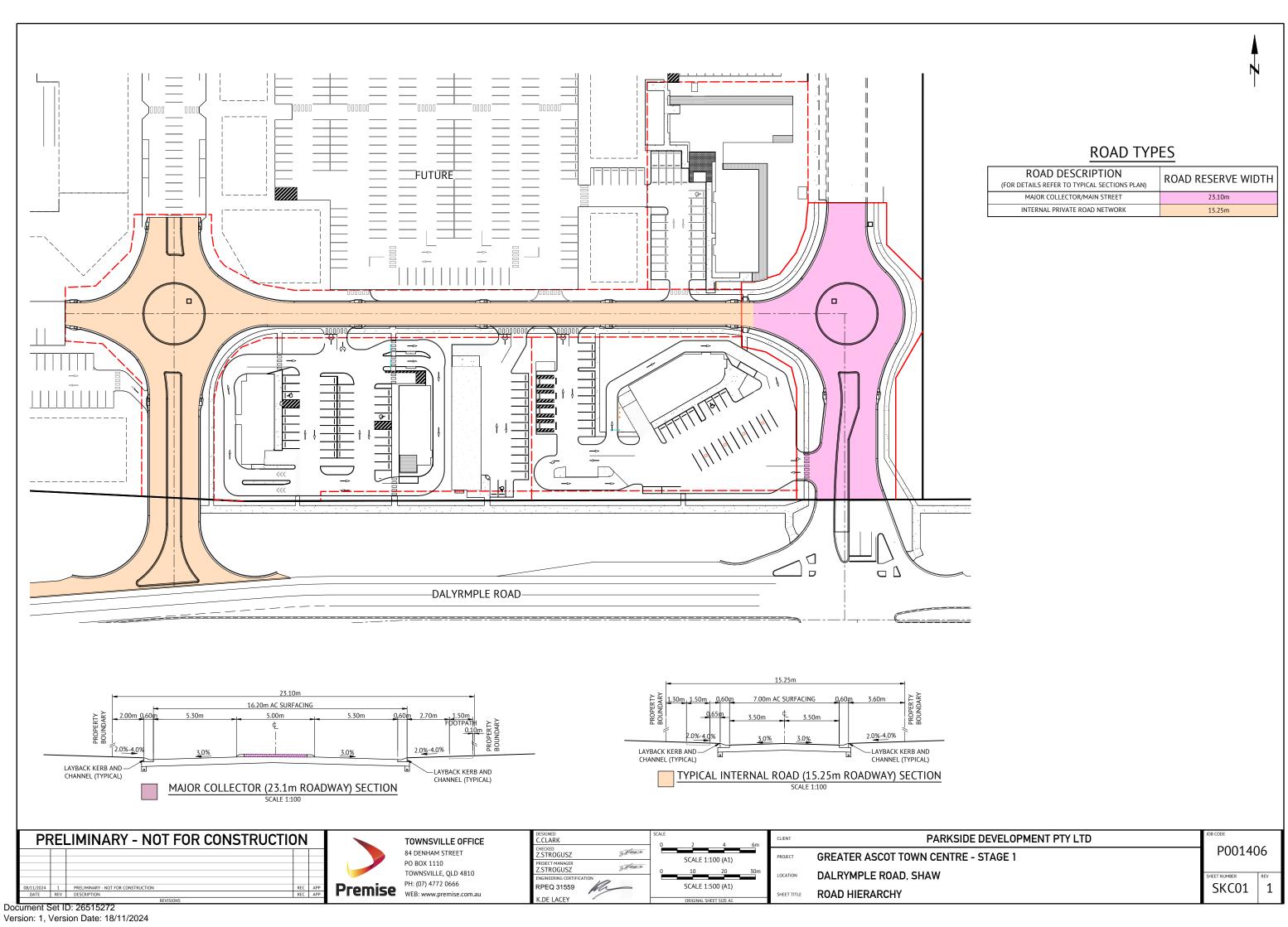
A review of the services proposed for this development and their impact on surrounding services, indicates that there is no impediment to development. The development can be adequately serviced by the existing water and sewer networks and electrical and telecommunications are also available within the vicinity of the site. The proposed minor and major drainage networks are in line with existing overall stormwater management plans approved for this development.



APPENDIX A

ROAD HIERARCHY AND CROSS SECTION PLAN

PAGE 14 | GREATER ASCOT TOWN CENTRE STAGE 1

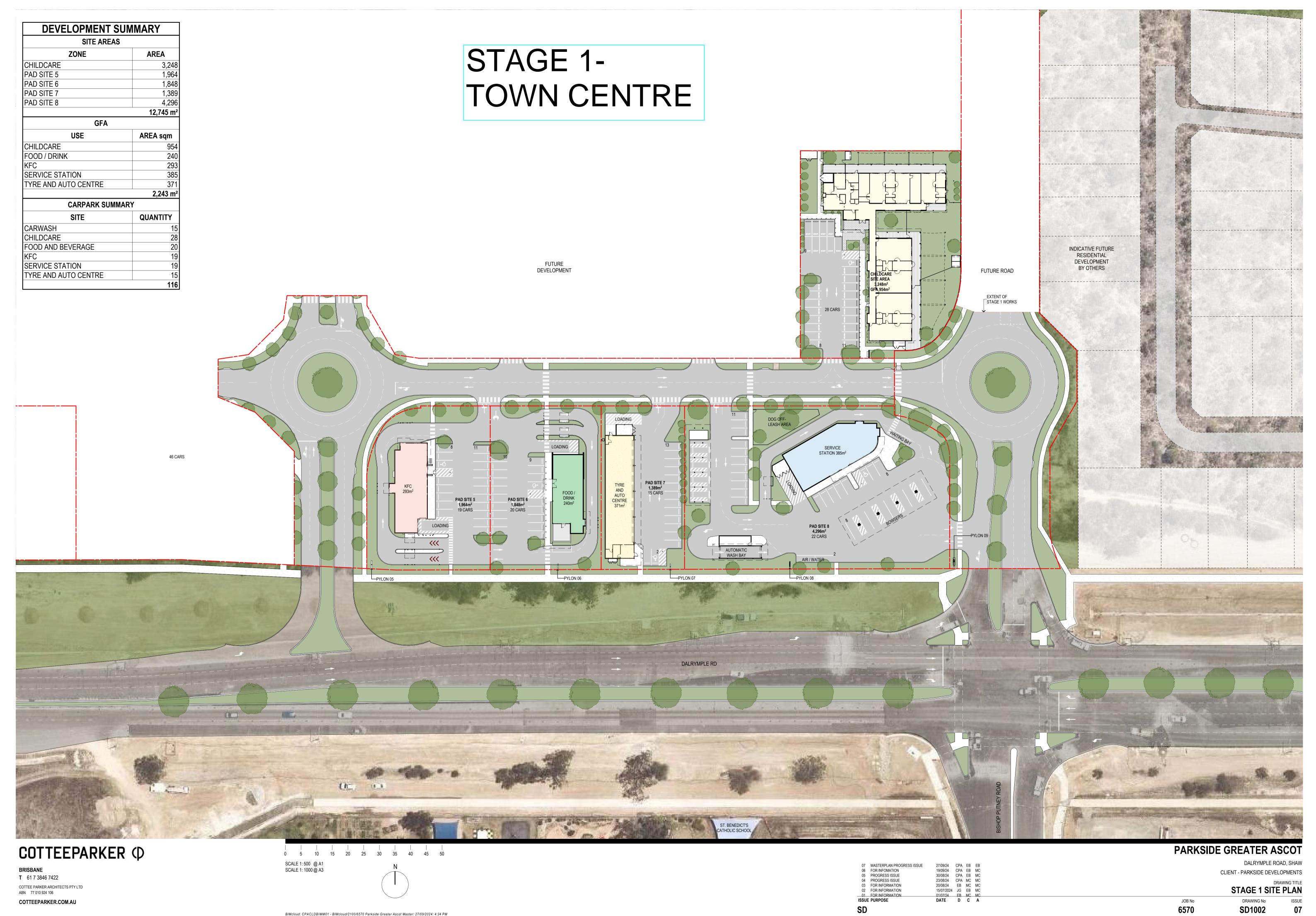


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APPENDIX B DEVELOPMENT SITE PLAN

PAGE 15 | GREATER ASCOT TOWN CENTRE STAGE 1





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DALRYMPLE ROAD, SHAW CLIENT - PARKSIDE DEVELOPMENTS

DRAWING TITLE

MASTERPLAN

DRAWING No

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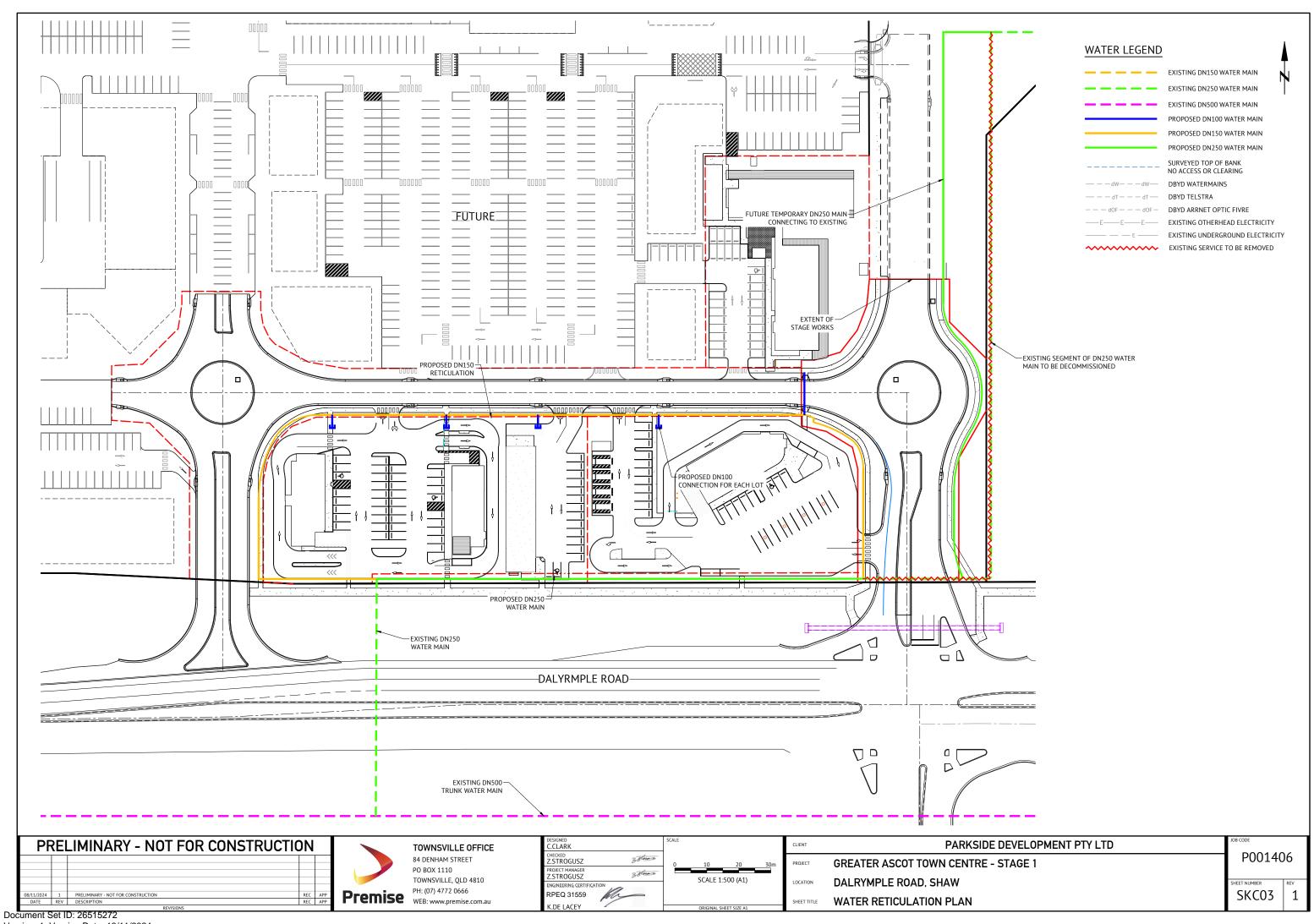
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APPENDIX C

CONCEPTUAL WATER NETWORK LAYOUT

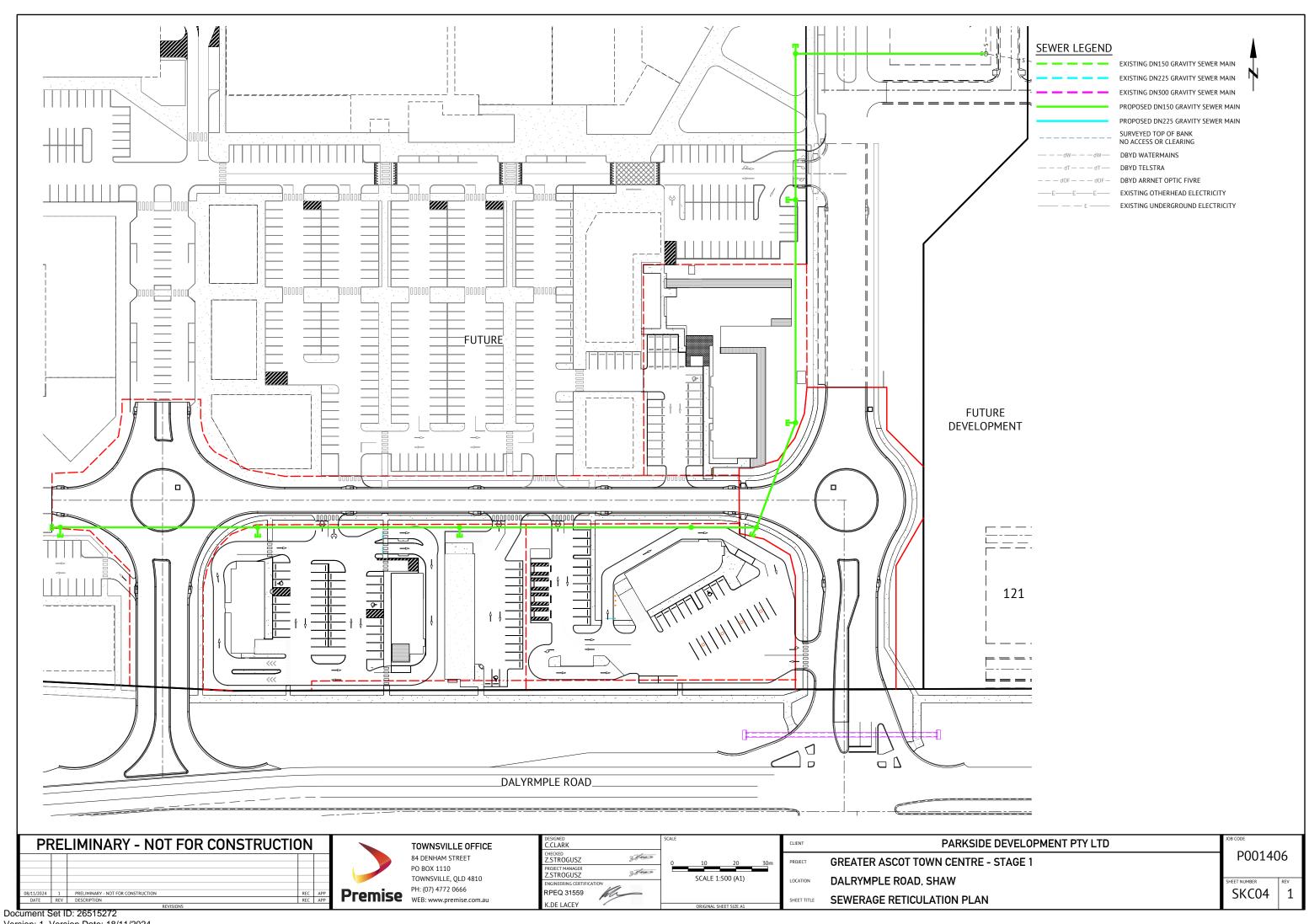
PAGE 16 | GREATER ASCOT TOWN CENTRE STAGE 1





APPENDIX D CONCEPTUAL SEWER LAYOUT

PAGE 17 | GREATER ASCOT TOWN CENTRE STAGE 1

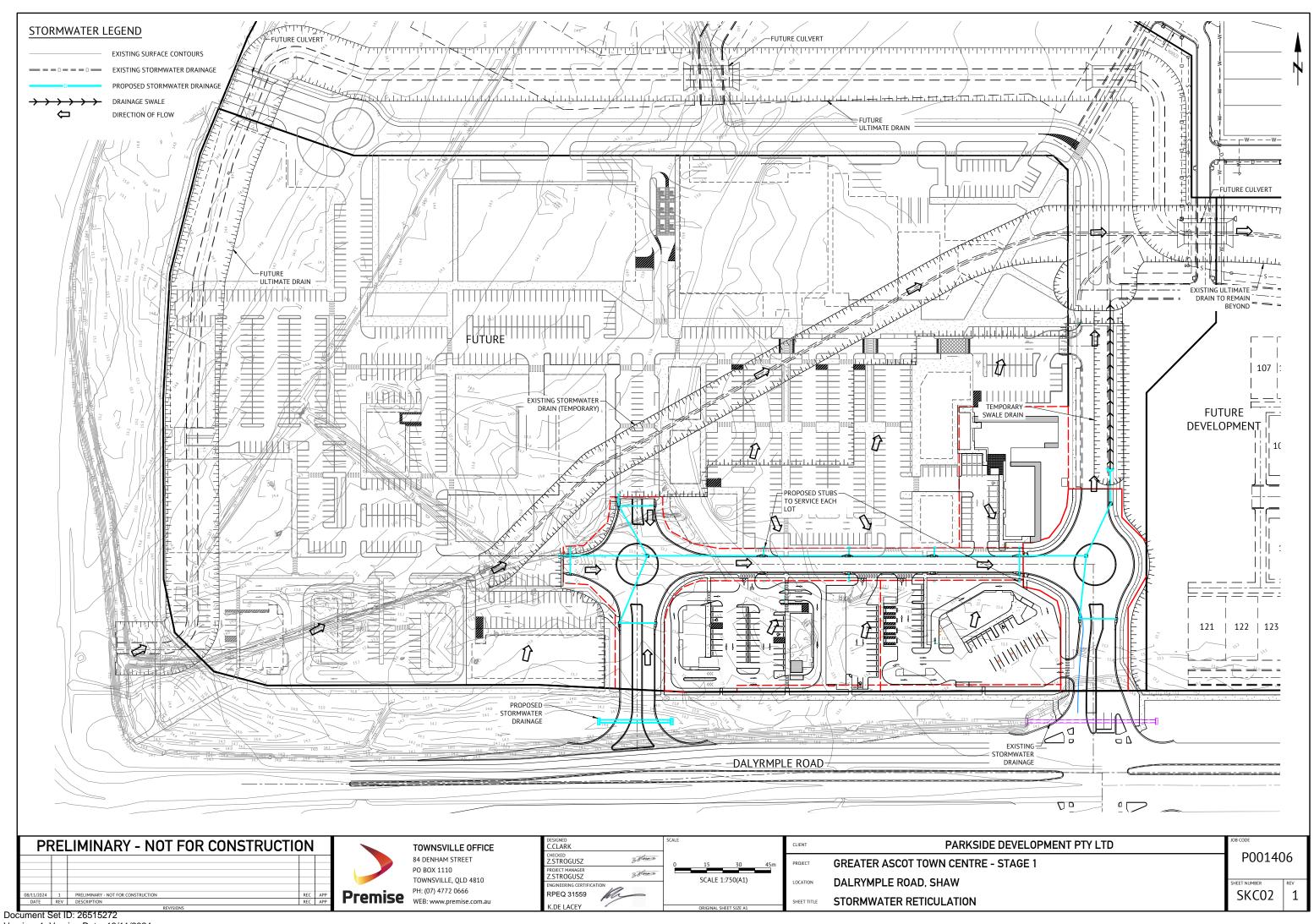




APPENDIX E

PROPOSED STORMWATER LAYOUT

PAGE 18 | GREATER ASCOT TOWN CENTRE STAGE 1





APPENDIX F

STORMWATER QUALITY MANAGEMENT PLAN

PAGE 19 | GREATER ASCOT TOWN CENTRE STAGE 1



STORMWATER QUALITY MANAGEMENT PLAN

Report No: P001406.R03

Rev: A

7 November 2024





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DOCUMENT AL	DOCUMENT AUTHORISATION						
Revision	Revision Date	Proposal D	etails				
Α	07/11/24	For Approv	For Approval				
Prepared By		Reviewed By		Authorised By			
Lawrence Mills	lij	Zac Strogusz	3 dines	Katie De Lacey	M		



CONTENTS

INTRODUCTION	1
EXISTING SITE	1
PROPOSED DEVELOPMENT	1
Stormwater Quality	1
Water Quality Objectives	2
MUSIC Modelling	2
Treatment Strategy	3
Pollutant Load Assessment	4
RECOMMENDATION	5
Table 1 – Catchment Characteristics	3
Table 2 – Bioretention Parameters	
Table 3 – Summary of MUSIC Results	
Table 4 – Bioretention Construction Costs	
FIGURES	
Figure 1 - Model Schematic (MUSIC)	ว

APPENDICES

Appendix A Development Site Plan Appendix B Preliminary Stormwater Drainage Layout Plan Appendix C Bio Retention Layout Plans and Costs



INTRODUCTION

Premise Townsville Pty Ltd has been commissioned by Parkside Developments Pty Ltd to prepare a Stormwater Quality Management Plan for Stage 1 of the Greater Ascot Town Centre on Lot 2 on SP 107219.

Townsville City Council has consistently provided support for stormwater quality management strategies that involved a monetary contribution toward catchment-wide off-site stormwater quality management infrastructure, for similarly sized developments of a similar nature. It is requested that a monetary contribution be accepted for this development's Stormwater Quality Management Strategy.

EXISTING SITE

The site (Stage 1 of Town Centre) is generally a greenfield site with undeveloped land and is zoned as "Emerging Community" under the TCC Planning Scheme. Land use surrounding the site is generally low to medium density residential. The site is currently unoccupied, consisting of cleared land, situated on the outer South Western corner of Greater Ascot Residential Development.

PROPOSED DEVELOPMENT

The proposed development (Stage1) will consist of five lots which will consist of the following commercial uses:

- > A service station, including a convenience store and carwash.
- > A car service centre.
- > Two (2) fast-food restaurants.
- A childcare centre site.

The proposed development will also consist of an internal road network consisting of two (2) roundabouts, which will be connected to future stages of the Greater Ascott Town Centre. Each of the above commercial facilities are expected to implement their own Stormwater Treatment devices and are not considered within the scope of this Stormwater Quality Plan. The catchment considered as part of this plan, will consist only of the internal road network which is estimated to comprise an area of 0.91 Ha.

Stormwater Quality

Current best practice Water Sensitive Urban Design (WSUD) techniques and solutions shall be employed during detailed design to ensure adverse impacts are minimised in accordance with the State Planning Policy (December 2013) and in association with Townsville City Council's WSUD for the Costal Dry Tropics (Townsville) Technical Guidelines (2011).



WATER QUALITY OBJECTIVES

The impact of the proposed development was evaluated in terms of long-term average annual pollutant loadings for a traditional residential site. This was accomplished by:

- > Establishing long-term base line pollutant loads from a Model for Urban Stormwater Improvement Conceptualisation (MUSIC) model of the current land uses in the catchment;
- > Modifying the baseline MUSIC model to incorporate the effects of the development due to changes in land use of the proposed development; and
- > Examining the relative increase / decrease in long-term pollutant loads to the receiving waters.

The major pollutants associated with the proposed development are total suspended solids, total Nitrogen, total Phosphorus and gross pollutants.

Townsville City Council requires reduction in pollutants generated from the developed site as detailed below:

- > Total suspended solids 80%;
- > Total Phosphorus 65%;
- > Total Nitrogen 40%; and
- > Gross pollutants 90%.

MUSIC MODELLING

MUSIC is a water quality modelling system developed by the Cooperative Research Centre for Catchment Hydrology (CRCCH). MUSIC can simulate runoff quantity and quality for catchments ranging in scale from a single residential lot to several square kilometres. MUSIC is widely suited to assessing the effectiveness of the proposed stormwater controls.

The latest version of MUSIC (v6.3.3) was used to analyse the proposed stormwater controls in this development.

The following data was used as input for the MUSIC models:

- > Long term rainfall data was obtained from the Townsville AERO pluviometer (gauge number 032040) at a six (6) minute data interval for a representative period from 1990-1999;
- > Monthly aerial potential evapotranspiration data from the Townsville Aero pluviometer;
- > A commercial area was adopted as the land use; and
- > Generic pollutant export parameters for the identified land uses have been adopted from the MUSIC Modelling Guidelines (Water by Design, Version 1, 2010).

The development was modelled as one lumped catchment (roadway and vegetation). (The breakdown of split areas was equivalent to the overall lumped fraction impervious). The catchment drains to a single bio-retention basin. The catchment characteristics are summarised in Table 1 and a model schematic is shown in **Error! Reference source not found.**

Table 1 – Catchment Characteristics

Catchment	Land Use	Catchment Area (Ha)	% Impervious
Greater Ascott Town Centre Stage 1 – Internal Road	COMMERCIAL	0.91	75%



Figure 1 - Model Schematic (MUSIC)

TREATMENT STRATEGY

A treatment strategy for the proposed development has been determined. The proposed treatment strategy includes an end of line bioretention system. Table 2 summarises the parameters used for modelling the bioretention system in MUSIC.

Table 2 – Bioretention Parameters

	Parameter	Bioretention A
1	Surface Area (m²)	192
2	Extended detention depth (m)	0.3
3	Filter treatment area (m²)	140
4	Unlined filter media perimeter (m)	54
5	Saturated hydraulic conductivity (mm/hr)	200
6	Filter depth (m)	0.6
7	TN content of filter media (%)	800
8	Orthophosphate content of filter media (mg/kg)	30
9	Is the base lined?	No
10	Vegetated with effective nutrient removal plants	Yes
11	Overflow weir width (m)	5
12	Exfiltration rate (mm/hr)	0
13	If an exfiltration rate has been used, have node water balance losses been used in calculations of treatment train effectiveness	N/A

PAGE 3



	Parameter	Bioretention A
14	If exfiltration rate has been used is the exfiltration rate justified?	N/A
15	Underdrain present?	Yes
16	Submerged zone with carbon present?	Yes
17	Depth of submerged zone (m)	0.45
18	Confirmation that K and C* remain default	Yes

Further specifications are as follows:

- > Filter Medium Sandy Loam;
- > Transition layer 100mm thick coarse sand in accordance with WSUD TDG 2006;
- > Drainage layer 200mm 2-5mm gravel in accordance with WSUD TDG 2006; and
- > Underdrain System An under-drain system of slotted drainage pipes (100mm dia at 1.5m centres).

Note: Transition Layer comply with the following: Top of drainage layer is to be at least 100mm above the top of the pipe and filter media / drainage material to comply with the Drainage of Subsurface Water from Road – Technical Bulletin No 32 (VicRoads).

POLLUTANT LOAD ASSESSMENT

Table 3 summarises the MUSIC results by showing a comparison of the mean pollutant loads for the Treatment Strategy. Overall pollutant loads have been reported at the downstream extent of the model.

Developed **Developed Case with Pollutant** treatment Case **Pollutant** Reduction **Residual Load and Percentage Targets Annual Load** Reduction **Total Suspended Solids** 1500 194 80% 87.1 % (kg/yr) Total Phosphorus (kg/yr) 4.07 1.28 68.5 % 65% Total Nitrogen (kg/yr) 23.7 9.55 59.6 % 40% 148 100 % 90% Gross Pollutants (kg/yr)

Table 3 – Summary of MUSIC Results

The model results indicate the developed case of the site with treatment devices to be:

- Overall Total Suspended Solids loads are reduced by approximately 87%;
- > Total Phosphorus loads are reduced by approximately 68%;
- > Total Nitrogen loads are reduced by approximately 60%; and
- > Gross Pollutant loads are reduced by 100%.

This indicates that the proposed bioretention has been adequately sized to satisfy the minimum reduction targets, as specified by Townsville City Council.

PAGE 4



RECOMMENDATION

In line with advice provided by Townsville City Council for similar developments of comparable size, it is proposed that bioretention infrastructure is not implemented on the subject site as a part of this development. For this development:

- a) The provision of on-site stormwater quality management infrastructure is not a cost-effective means of achieving stormwater quality outcomes for the developer;
- The maintenance costs associated with any on-site stormwater quality management infrastructure is not a cost-effective means for Council to achieve stormwater quality outcomes;
- Any on-site stormwater quality management infrastructure that is provided on-site will be a less effective means of achieving stormwater quality outcomes than an offsite solution that could treat water from the broader catchment; and

A monetary contribution toward the implementation of catchment-wide stormwater quality management infrastructure, or the preparation of plans for such infrastructure, is recommended to be the most efficient and effective way to realise stormwater quality improvement for the catchment.

Table 4 below summarises construction details of recent bioretention basins built in Townsville over the past year including development name, treatment areas, construction costs, and the calculated cost per m² of filter/treatment area. The construction costs include earthworks, drainage structures, subsoil drains, filter material and temporary turfing, topsoil & geofabric for each bioretention. The Temporary turfing, topsoil and geofabric is not required when the bioretention is constructed to its ultimate form and therefore the temporary works are considered equal in value to the planting out of the basin treatment surface area.

Error! Reference source not found. contains the bioretention basins civil layout plans and extracts from the progress claims for each of the developments listed in Table 4.

Table 4 – Bioretention Construction Costs

Development	Basin Filter Treatment Area m2 (Approx.)	Total Construction Cost (2023/2024)		Cost per m ² of Filter Treatment Area		
ELLIOT SPRINGS - WHITES CREEK STAGES 37 TO 40 - BASIN A	570	\$	206,425.00	\$	362.15	
ELLIOT SPRINGS - WHITES CREEK STAGES 37 TO 40 -BASIN B	230	\$	91,238.00	\$	396.69	
ELLIOT SPRINGS - WHITES CREEK STAGES 10 -14 - BASIN C	410	\$	177,660.00	\$	433.32	
ELLIOT SPRINGS - WHITES CREEK STAGES 10 -14 - BASIN D	1055	\$	383,555.00	\$	363.56	



Development	Basin Filter Treatment Area m2 (Approx.)	Total Construction Cost (2023/2024)		Cost per m² of Filter Treatment Area		
ELLIOT SPRINGS - WHITES CREEK STAGES 10 -14 - BASIN E	208	\$	122,009.00	\$	586.58	
GREATER ASCOT STAGES 804 805 806 - BASIN A	380	\$	124,545.00	\$	327.75	
GREATER ASCOT STAGES 804 805 806 - BASIN B	335	\$	110,033.00	\$	328.46	
RIVERSTONE - BASIN A	270	\$	74,457.00	\$	275.77	
RIVERSTONE - BASIN B	620	\$	127,857.00	\$	206.22	
Total	4078m ²	\$ 1,417,779.00		\$347.	65/m²	

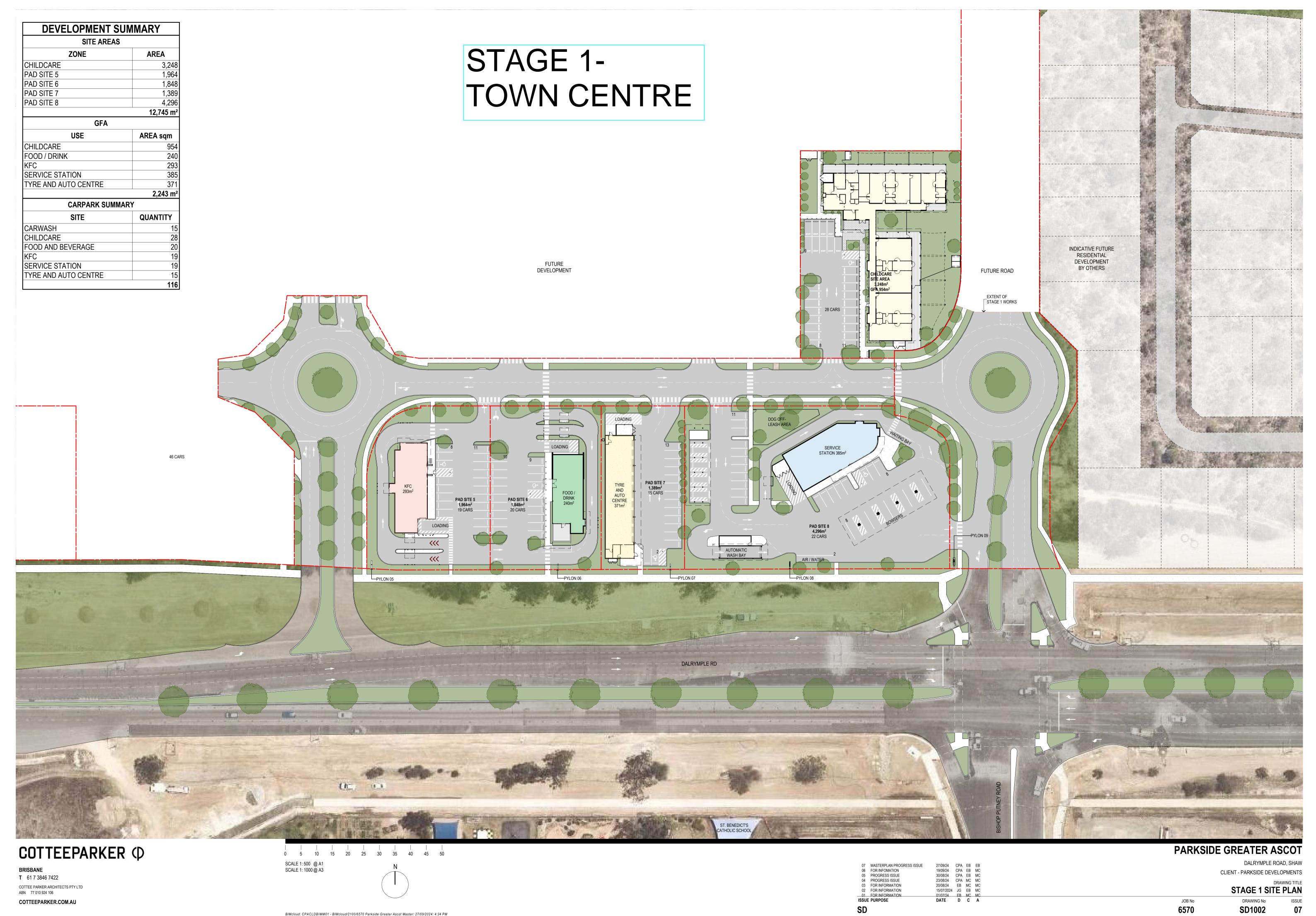
Based on the developments listed in Table 4 it is determined that the average construction cost per m² of Filter treatment area for a bioretention basin in Townsville is approximately \$347.65/m².

The cost of providing stormwater treatment facilities for the Stage 1 of the Greater Ascott Town Centre, proportionate to the approved land area has been calculated as 140m² (Table 2, Row 3) basin filter treatment area, multiplied by average construction cost per m² \$347/m2, \$48,580.00 excl GST.

It is recommended that the developer and council enter into an Infrastructure Agreement based on the above calculated costs and the developer makes a monetary contribution to Townsville City Council to offset any stormwater quality requirements of the development.

Appendix A

Development Site Plan





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DALRYMPLE ROAD, SHAW CLIENT - PARKSIDE DEVELOPMENTS

DRAWING TITLE

MASTERPLAN

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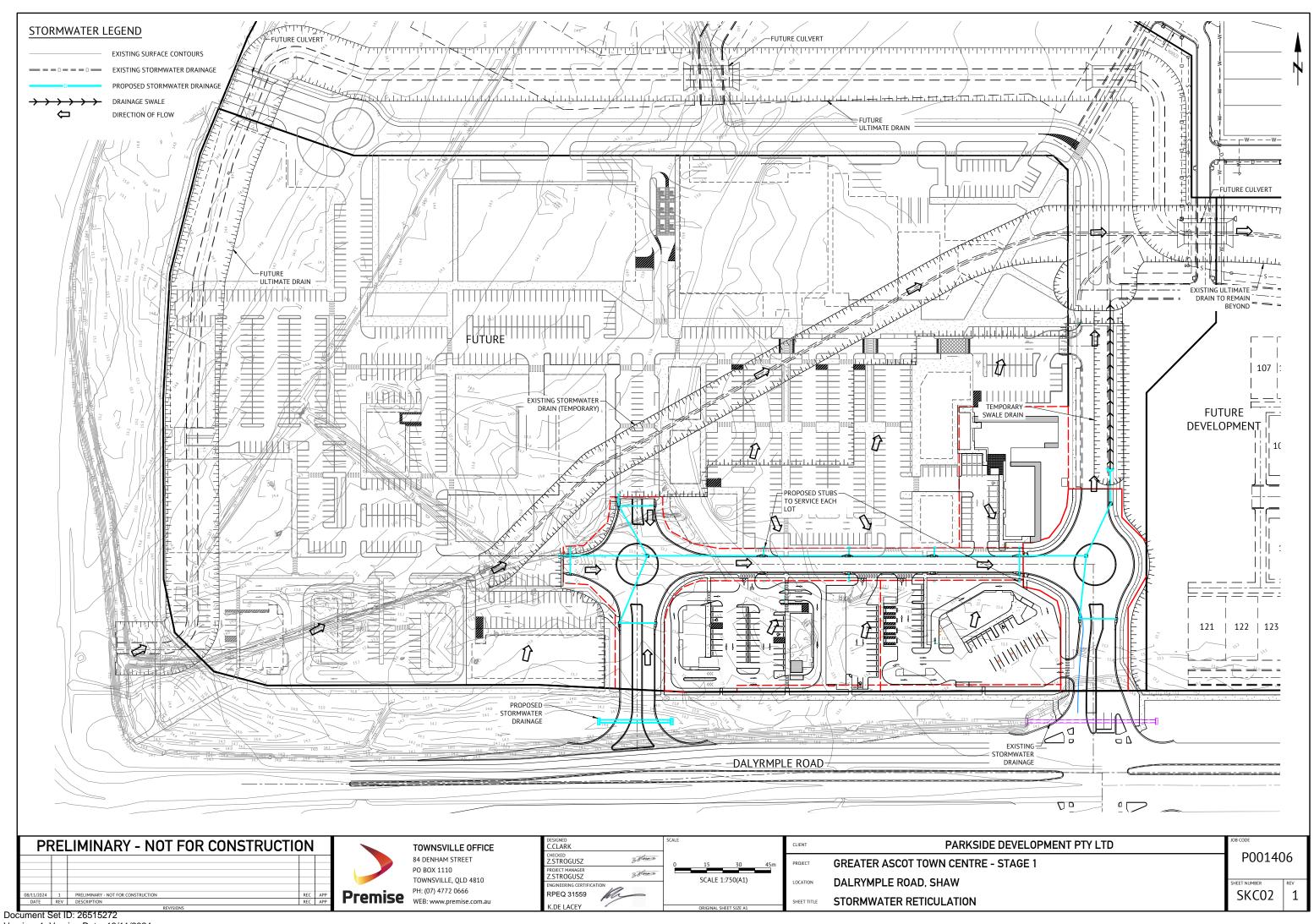
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Appendix B

Preliminary Stormwater Drainage Layout Plan

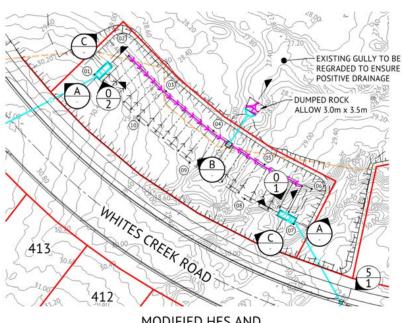


Appendix C

Bio Retention Layout Plans and Costs

	BASIN A - BASE AREA 615m2					
	ELLIOT SPRINGS - WHITES CREEK STA	GES 37 TO 40	LLC-0093	SEPT 2024		
Item	Description	Unit	Quantity	Contract Rate	Contract Amount	
4	Scour Protection					
(a)	Dumped rock - 600 mm thick (D_{50} 300 mm) on geotextile fabric (Bidum A34)	m ²	11	\$ 45.25	\$ 497.75	
5	Bio-Retention drainage works including subsoil drainage, filter media and temporary turfing					
(a)	Bio-Retention A - including excavate 300mm below filter media profile, place geofabric and installation of floculation unit and floculant	m ²	600	\$ 183.60	\$ 110,160.00	
(b)	Bio-Retention A - preparation of subgrade, installation of all drainage pipes and filter media, geofabric, topsoil and turf	m²	600	\$ 117.23	\$ 70,338.00	
7	Supply and construct cast in situ concrete headwall, wingwall and apron to match the following RCBC sizes					
(a)	Bio-retention headwall including wingwalls and course sediment forebay	Each	2.0	\$ 11,259.51	\$ 22,519.02	
(a)	Hydromulching H2	m ²	990	\$ 2.94	\$ 2,910.60	
					\$ 206,425.37	

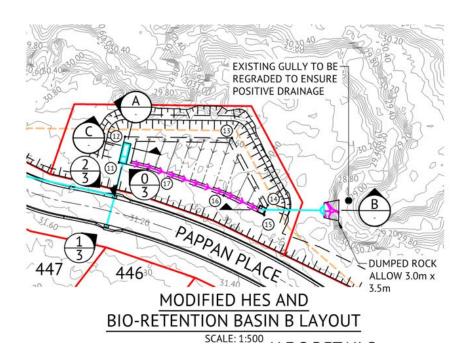
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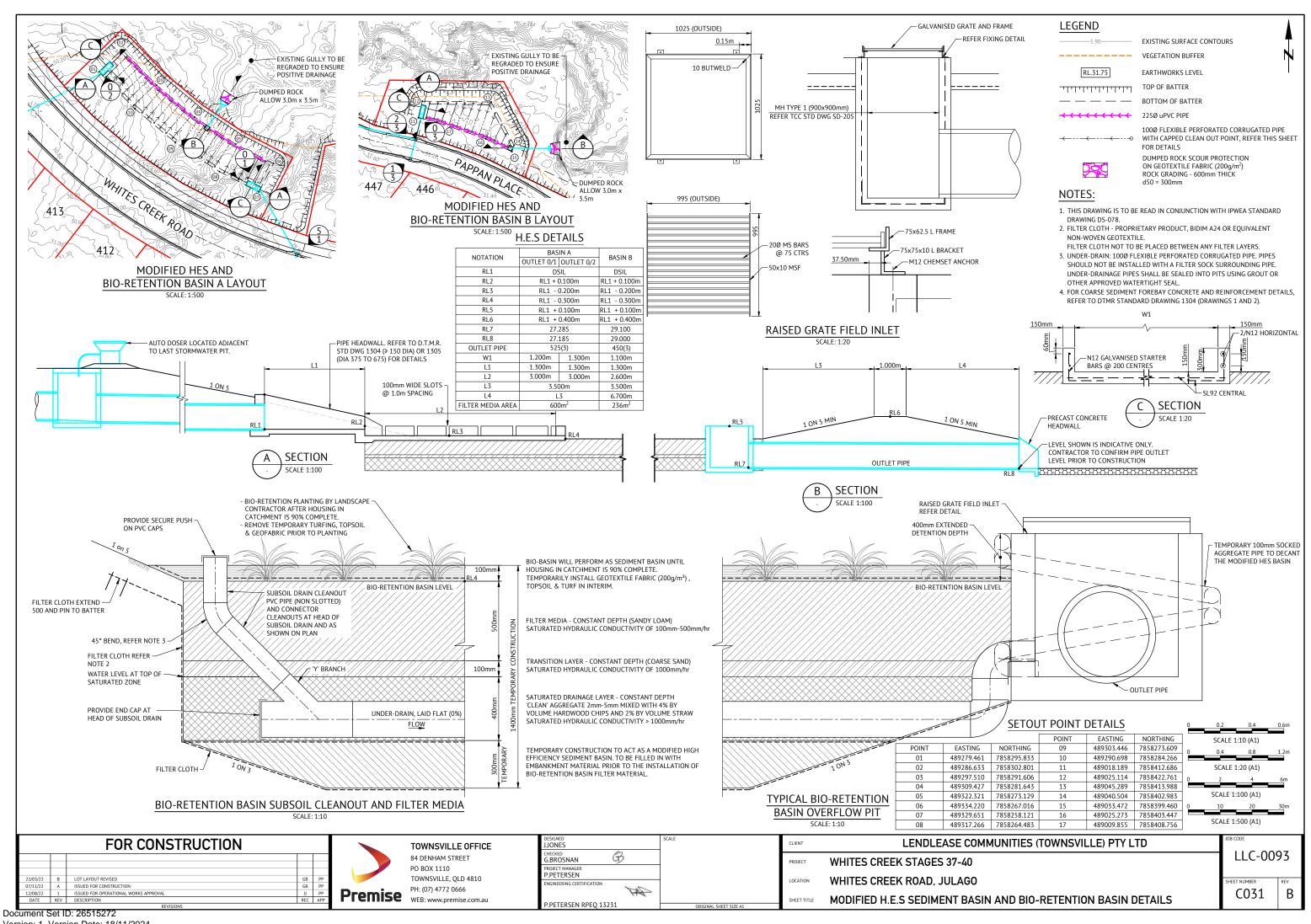


MODIFIED HES AND
BIO-RETENTION BASIN A LAYOUT
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	BASIN B - BASE AREA 245 m2					
	ELLIOT SPRINGS - WHITES CREEK STA	GES 37 TO 40	LLC-0093	SEPT 2024		
Item	Description	Unit	Quantity	Contract Rate	Contract Amount	
4	Scour Protection					
(a)	Dumped rock - 600mm thick (D ₅₀ 300mm) on geotextile fabric (Bidum A34)	m ²	11	\$ 45.25	\$ 497.75	
5	Bio-Retention drainage works including subsoil drainage, filter media and temporary turfing					
(c)	Bio-Retention B - including excavate 300mm below filter media profile, place geofabric and installation of floculation unit and floculant	m ²	236	\$ 209.15	\$ 49,359.40	
(d)	Bio-Retention B - preparation of subgrade, installation of all drainage pipes and filter media, geofabric, topsoil and turf	m²	236	\$ 122.90	\$ 29,004.40	
7	Supply and construct cast in situ concrete headwall, wingwall and apron to match the following RCBC sizes					
(a)	Bio-retention headwall including wingwalls and course sediment forebay	Each	1.0	\$ 11,259.51	\$ 11,259.51	
(a)	Hydromulching H2	m ²	380	\$ 2.94	\$ 1,117.20	
					\$ 91,238.26	

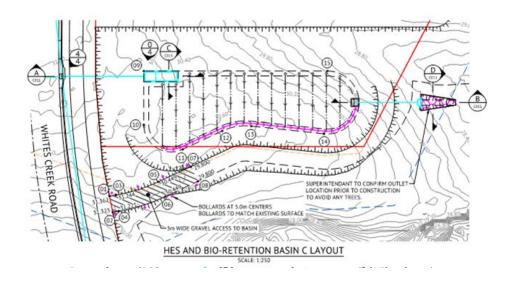
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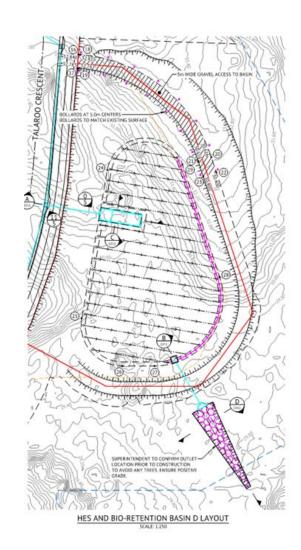
	BASIN C - BASE 440m2					
ELI	IOT SPRINGS - WHITES CREEK STAGES 10 -14	LLC-0095 TEN	NDERS ONL	Υ		
Item	Description	Unit	Quantity	Rate	Amount	
3	Scour Protection					
(a)	Dumped rock - 500mm thick (D ₅₀ 200mm) on geotextile fabric (Bidrum A34)	m ²	13	\$ 69.90	\$ 908.70	
4	Bio-Retention drainage works including subsoil drainage, filter media and temporary turfing					
(a)	Bio-Retention C - including excavate 300mm below filter media profile, place geofabric and installation of floculation unit and floculant	m²	440	\$ 68.99	\$ 30,355.60	
(b)	Bio-Retention C - preparation of subgrade, installation of all drainage pipes and filter media,	m ²	440	\$ 282.63	\$ 124,357.20	
2	Supply and construct cast in situ concrete headwall, wingwall and apron to match the					
(a)	Bio-retention headwall including wingwalls and course sediment forebay	Each	1	\$ 22,039.30	\$ 22,039.30	
2	LANDSCAPING Earthworks					
					\$ 177,660.80	

taken from Tender



BASIN D - BASE 1135m2 ELLIOT SPRINGS - WHITES CREEK STAGES 10 - 14 LLC-0095 TENDERS ONLY Description Unit Quantity Rate Item Amount 3 Scour Protection (a) Dumped rock - 500mm thick (D₅₀ 200mm) on geotextile fabric (Bidrum A34) m^2 69.90 61 4,263.90 Bio-Retention D - including excavate 300mm (c) below filter media profile, place geofabric and m² installation of floculation unit and floculant 1135 46.06 52,278.10 (d) Bio-Retention D - preparation of subgrade, m² installation of all drainage pipes and filter media, 268.70 304,974.50 1135 2 Supply and construct cast in situ concrete headwall, wingwall and apron to match the (a) Bio-retention headwall including wingwalls and course sediment forebay Each \$ 22,039.30 22,039.30 2 LANDSCAPING Earthworks \$ 383,555.80

taken from Tender

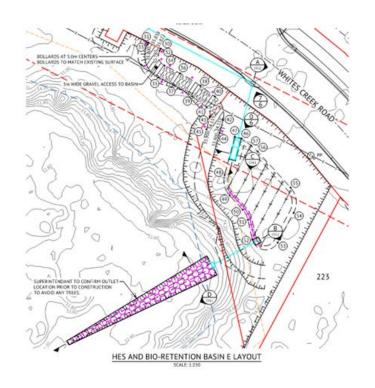


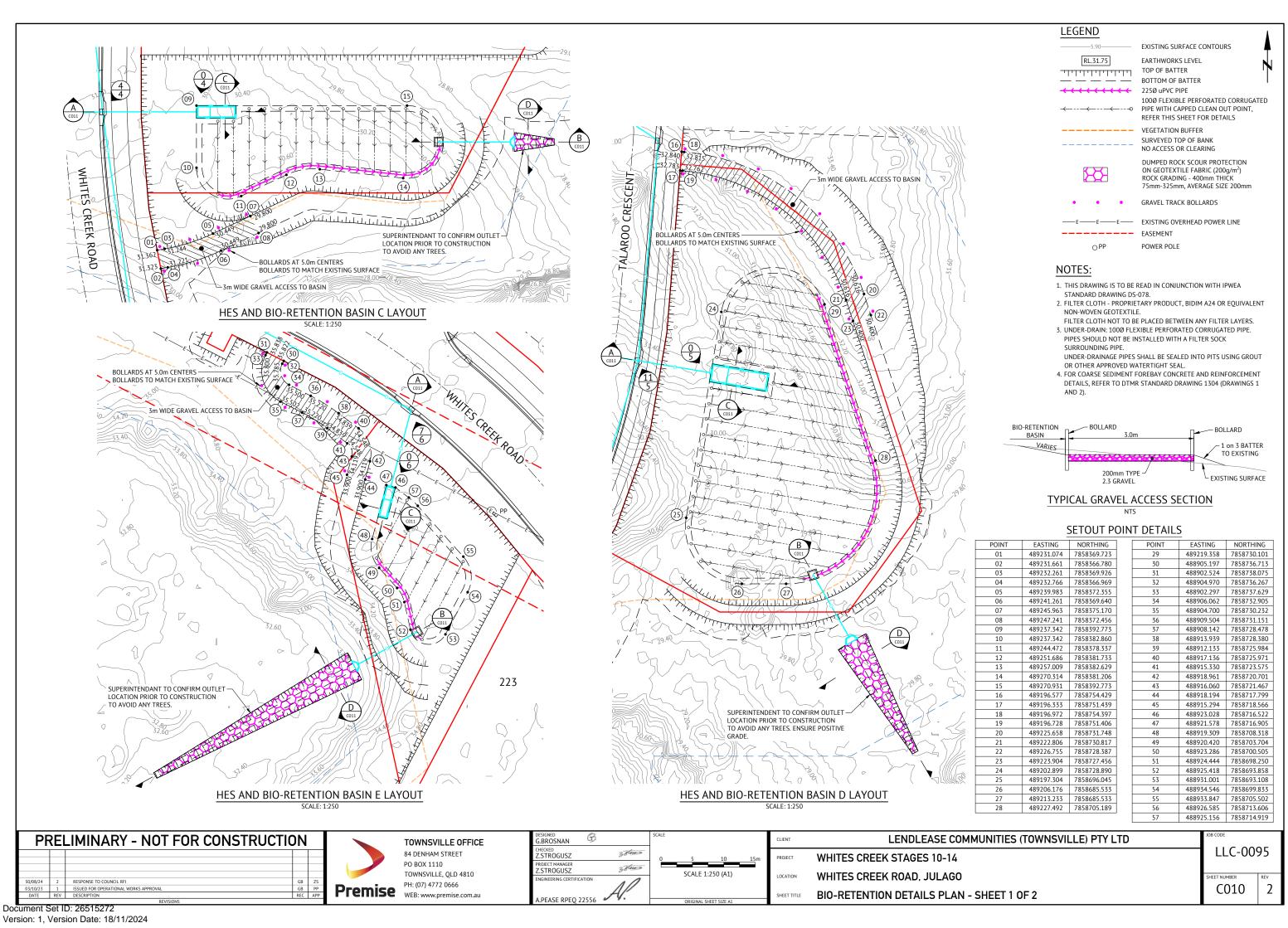
BASIN E - BASE 224m2

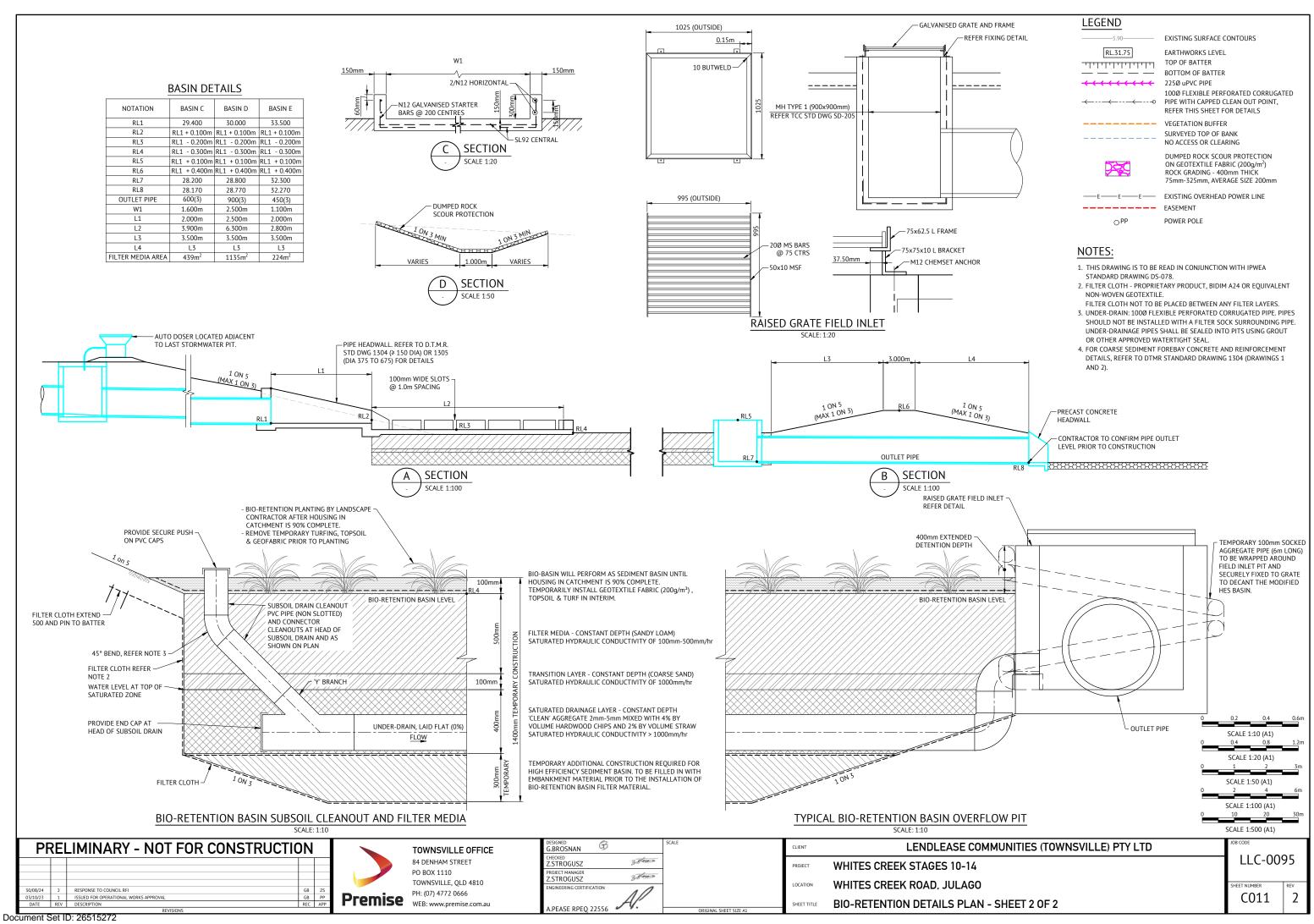
ELLIOT SPRINGS - WHITES CREEK STAGES 10 -14 LLC-0095 TENDERS ONLY

Item	Description	Unit	Quantity	Rate	Amount
3	Scour Protection				
(a)	Dumped rock - 500mm thick (D ₅₀ 200mm) on geotextile fabric (Bidrum A34)	m²	106	\$ 69.90	\$ 7,409.40
(f)	Bio-Retention E - preparation of subgrade, installation of all drainage pipes and filter media, geofabric, topsoil and turf	m²	224	\$ 302.16	\$ 67,683.84
(e)	Bio-Retention E - including excavate 300mm below filter media profile, place geofabric and	m ²	224	\$ 111.06	\$ 24,877.44
2	Supply and construct cast in situ concrete headwall, wingwall and apron to match the following RCP sizes				
(a)	Bio-retention headwall including wingwalls and course sediment forebay	Each	1	\$ 22,039.30	\$ 22,039.30
					\$ 122,009.98

taken from Tender







	GREATER ASCOT STAGES 805 806	PAR0081			
Item	Description	Unit	Quantity	Rate	Amount
3	Revegetation including establishment				
(a)	Hydromulching -	m ²	350	\$ 7.60	\$ 2,660
4	Bio-Retention drainage works including subsoil drainage, filter media and temporary turfing				
(a)	Bio-Retention A - including excavate 300mm below filter media profile, place geofabric and installation of floculation unit and floculant	m²	410	\$ 60.00	\$ 24,600
(b)	Bio-Retention A - preparation of subgrade, installation of all drainage pipes and filter media, geofabric, topsoil and turf	m²	410	\$ 130.00	\$ 53,300
4	Field inlets complete including excavation and disposal of spoil				
(b)	Flush grate field inlet - 900mm x 900mm - Basin A & B	Each	1	\$ 6,585.00	\$ 6,585
6	Supply and construct cast in situ concrete headwall, wingwall and apron to match the following RCP sizes				
(a)	Bio-retention headwall including wingwalls and course sediment forebay - Basin - A	Each	1	\$ 36,500.00	\$ 36,500
6	Scour Protection				
(a)	Dumped Rock - 400mm thick (DN 200mm) on geotextile fabric (200g/m2)	m ²	15	\$ 60.00	\$ 900.
					\$ 124,545.

taken from Claim 6

